



Design and Jitter Modeling of Energy Efficient High Speed Hybrid ADC



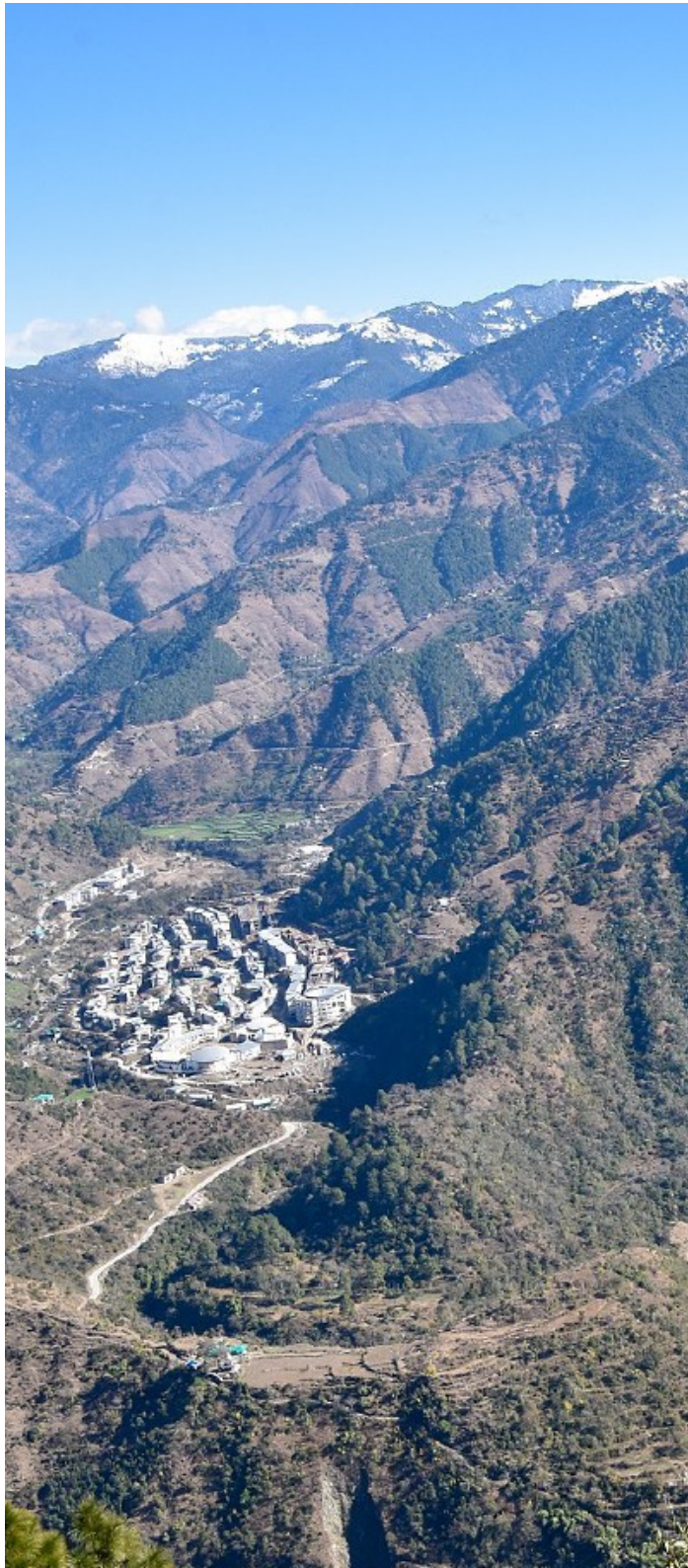
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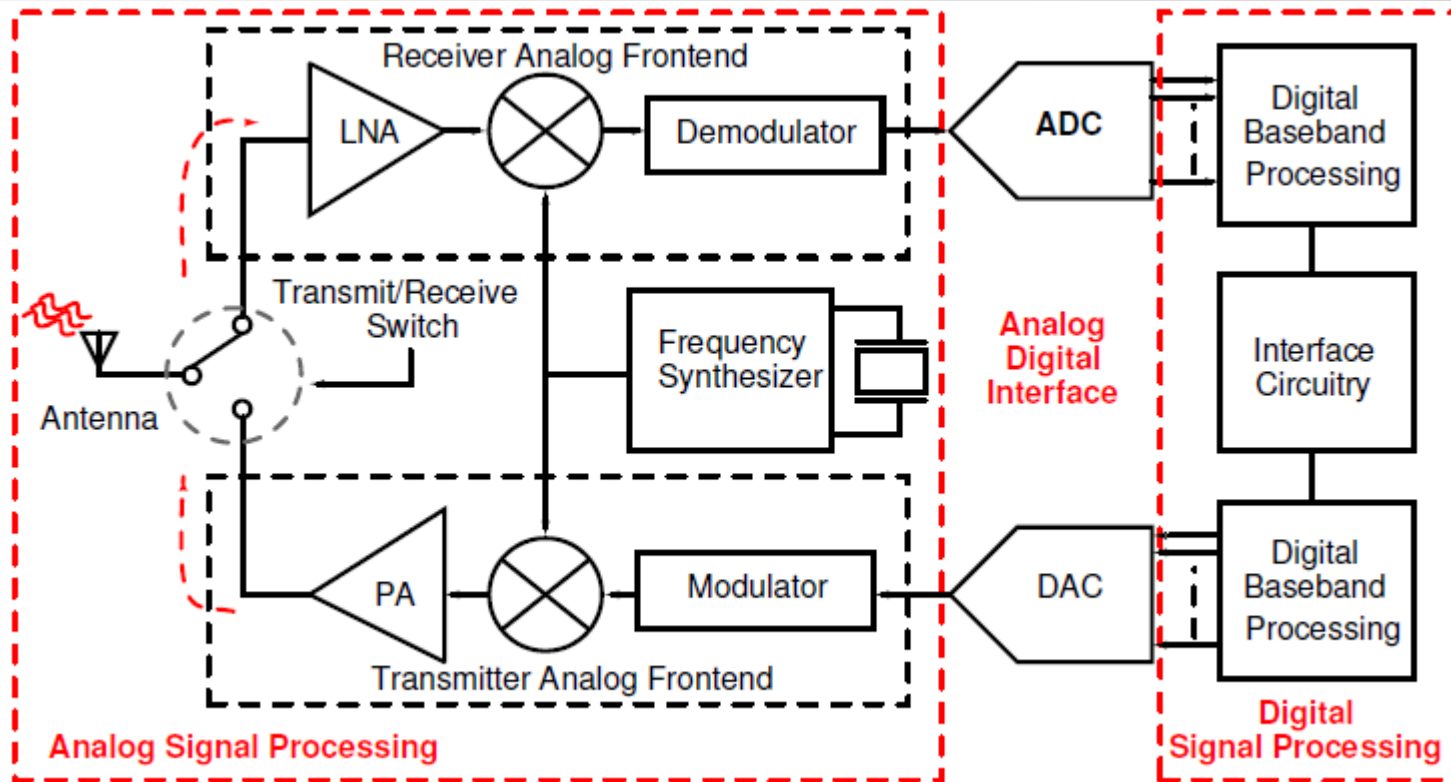








Transceiver



- Converts analog signals into digital bits.
- Synchronization by frequency synthesizer.
- Quantization by comparator circuitry.
- Code conversion by digital logic circuitry.

Selection of ADC

- The analog-to-digital converter (ADC) topology is chosen carefully to achieve the desired trade off between
 - Number of bits,
 - Sampling rate and
 - Power consumption
 - Flash ADC
 - SAR ADC
 - Pipelined ADC
 - Hybrid ADC
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Literature Survey

- Conversion energy of ADC is reduced by half every 2 years. ¹
- Speed of conversion increases by two folds every 4 years.
- 20 GS/s ADC with a power discipation of 1.2 W. ²
- Ethernet standard IEEE 802.3bj ³
 - 100 GS/s (4 X interleaved 25 GS/s)
 - 5–6 Effective Number of Bits (ENOB)
- Long range standard OTU-4
 - 100 GS/s (2 X interleaved 50 GS/s)
 - 5–6 Effective Number of Bits (ENOB)

¹Murmann, "Trends in low power digitally assisted A/D conversion", IEICE Trans. Electron, Jun. 2008.

²P. Schvan, et.al, "A 24 GS/s 6 b ADC in 90 nm CMOS," ISSCC Dig. Tech. Papers, 2008.

³L.Kull, et.al "A 3.1 mW 8b 1.2 GS/s single-channel asynchronous SAR ADC with alternating comparator for enhanced speed in 32 nm SOI CMOS ", IEEE JSSC, Dec. 2013

Literature Survey

- Time interleaving and multi-bit processing can lead to better efficiency. ⁴
- Time-interleaved (TI) ADCs are popular architectures that satisfy multi GS/s and high-resolution requirements ⁵
- SAR ADCs are superior in aspects of power efficiency and are highly scalable to an advanced CMOS technology ⁶
- Time-interleaved SAR ADC designed for 5 GS/s with 10 bits of resolution consumes 76 mW of power ⁷

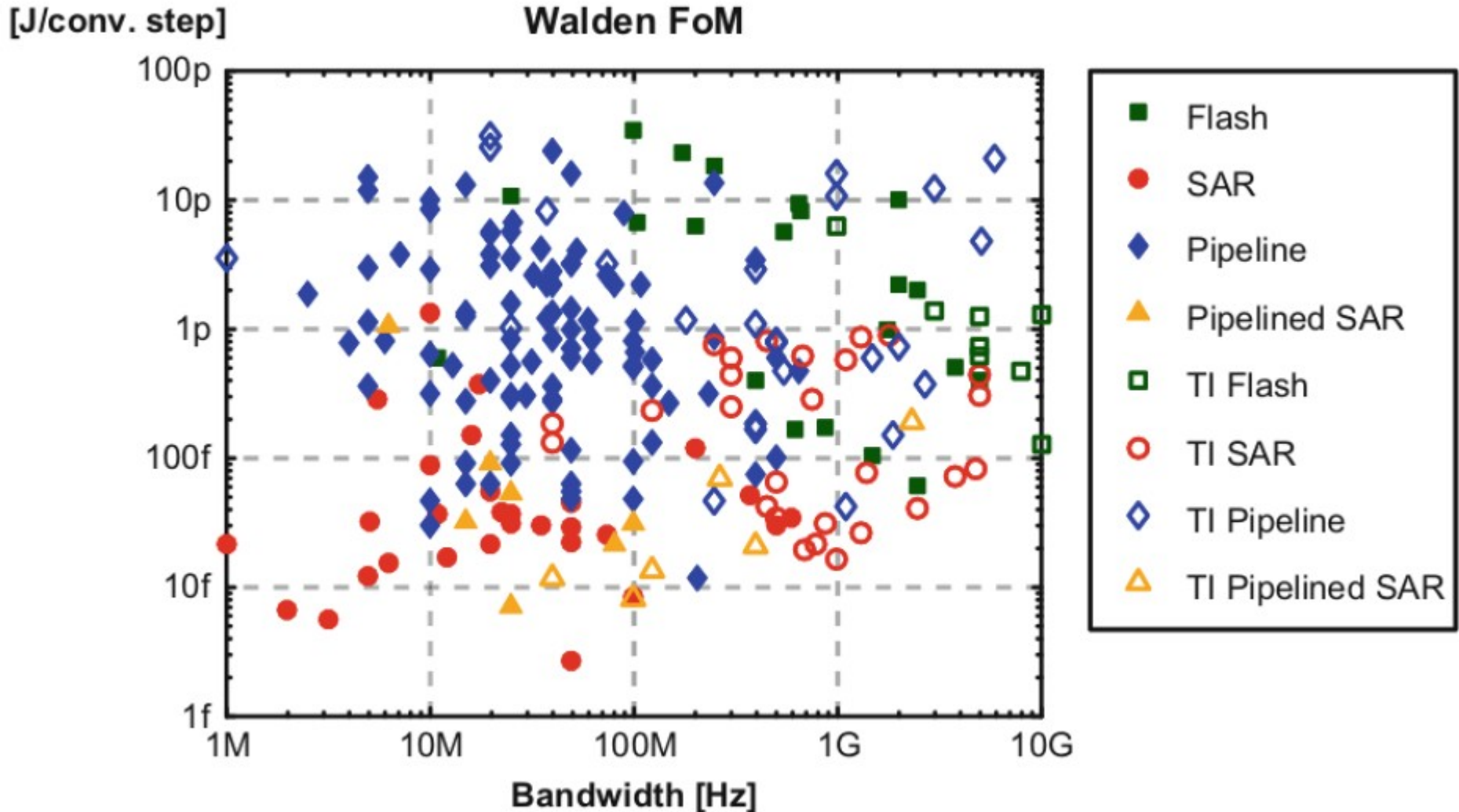
⁴C.H. Chan "A 5.5 mW 6b 5 GS/s 4xinterleaved 3b/cycle SAR ADC in 65 nm CMOS", ISSCC, Mar. 2015.

⁵K. Doris, et.al, "A 480 mW 2.6 GS/s 10b time-interleaved ADC with 48.5 dB SNDR up to Nyquist in 65 nm CMOS," IEEE JSSC, Dec. 2011

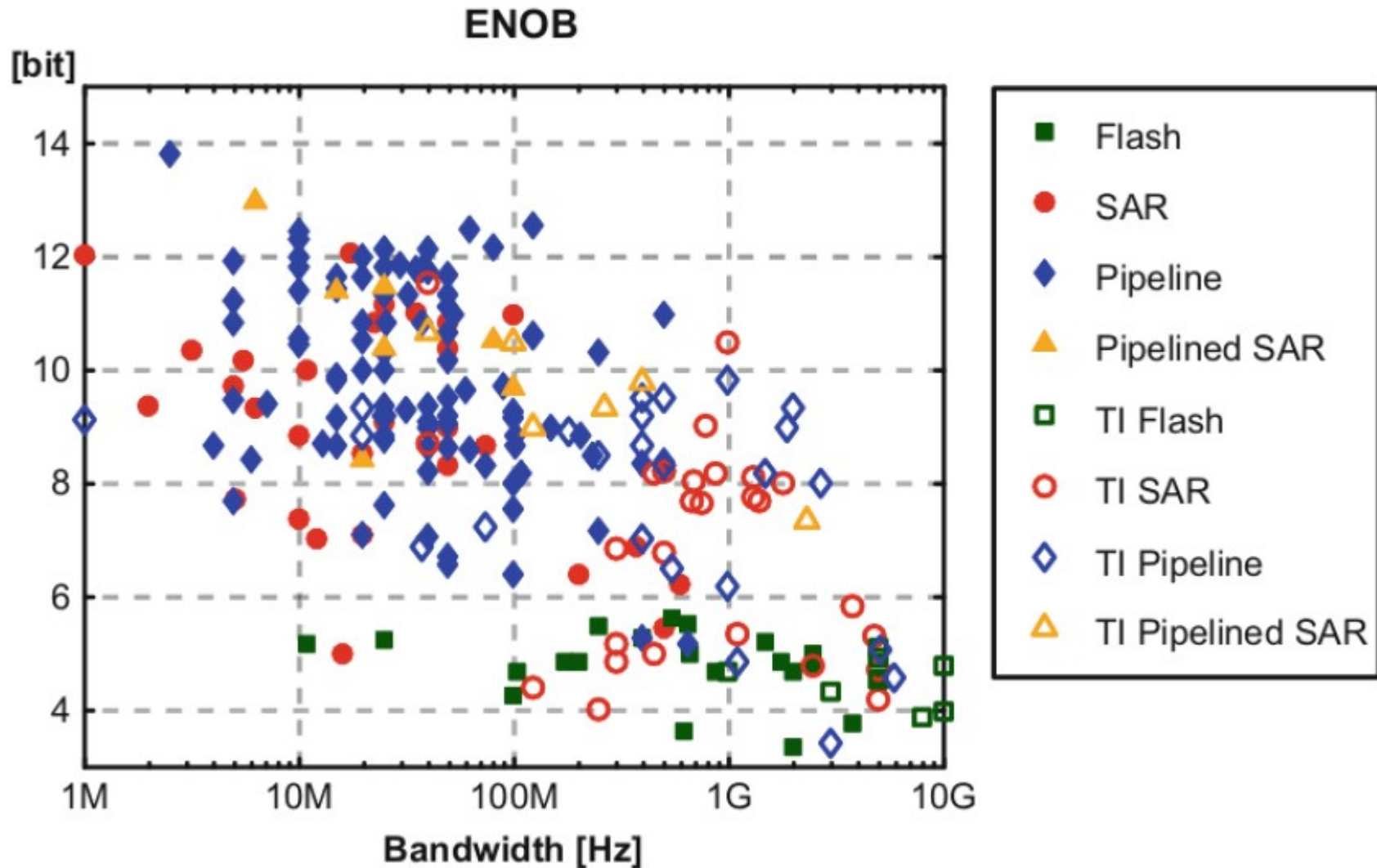
⁶M. Inerfield et al., "An 11.5-ENOB 100-MS/s 8mW dual-reference SAR ADC in 28nm CMOS," in Symp. VLSI Circuits (VLSI), Jun. 2014.

⁷J. Fang et.al "A 5-GS/s 10b 76-mW time interleaved SAR ADC in 28 nm CMOS" IEEE TCAS-I, Jul. 2017.

FOM: ISSCC 1997-2016



ENOB: ISSCC 1997-2016



Background

- Analog-to-digital converters (ADC) play an important role in the design of radio frequency (RF) transceiver architectures ⁸
- Hybrid ADC architectures exhibit excellent performance for analog and mixed signal (AMS) systems.
- Successive Approximation Register (SAR) ADC
 - Lower power consumption for higher resolution (N).
 - Medium speed ADC
 - Conversion Speed = N clock cycles
- Flash ADC
 - Higher bandwidth
 - Higher power consumption
 - Conversion speed = 1 clock cycle

⁸ S. Kundu, et.al, "A 1.2 V 2.64 GS/s 8-bit 39 mW skew-tolerant time-interleaved SAR ADC in 40 nm digital LP CMOS for 60 GHz WLAN," in IEEE CICC, Sep. 2014, pp. 1-4.

Aerial view

- Broad bandwidth techniques
 - Time interleaving ⁹
 - Alternating comparator ¹⁰
 - Multi-channel ADC techniques ¹¹
- Non-ideal effects
 - Offset Cancellation
 - Kickback noise reduction

⁹ B. P. Ginsburg and A. P. Chandrakasan, "500-MS/s 5-bit ADC in 65-nm CMOS with split capacitor array DAC," IEEE JSSC, vol. 42, no. 4, pp.739–747, Apr. 2007.

¹⁰ L. Kull, et.al "A 3.1 mw 8b 1.2 GS/s single-channel Asynchronous SAR ADC with Alternate Comparators for Enhanced speed in 32 nm Digital SOI CMOS," IEEE JSSC, vol. 48, no. 12, pp. 3049–3058, Dec. 2013.

¹¹ Z. Cao, et.al, "A 32 mW 1.25 GS/s 6-b 2b/step SAR ADC in 0.13 μ m CMOS," IEEE JSSC, vol. 44, no. 3, pp. 862–873, Mar. 2009.

Flash Architecture

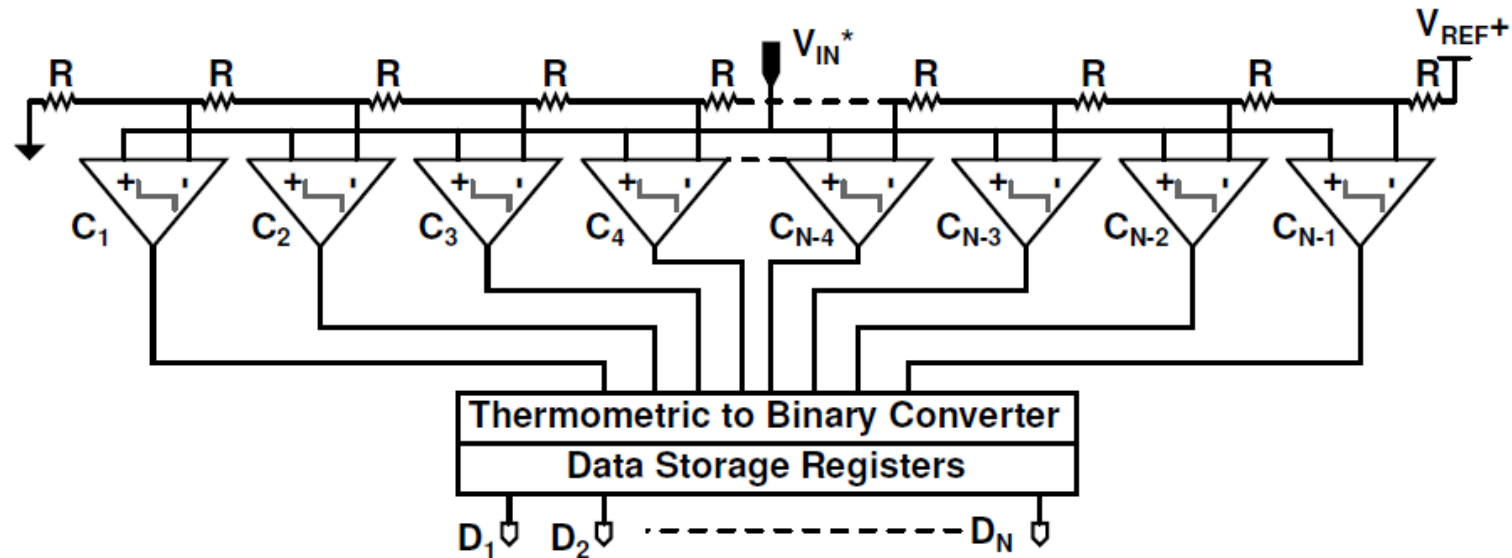


Figure: Block diagram of a flash analog-to-digital converter 12

- Increased bandwidth
- Higher power consumption
- Conversion cycles = 1 clock cycle
- Parallel processing architecture
- $2^N - 1$ comparators
- Comparator offset variation

SAR Architecture

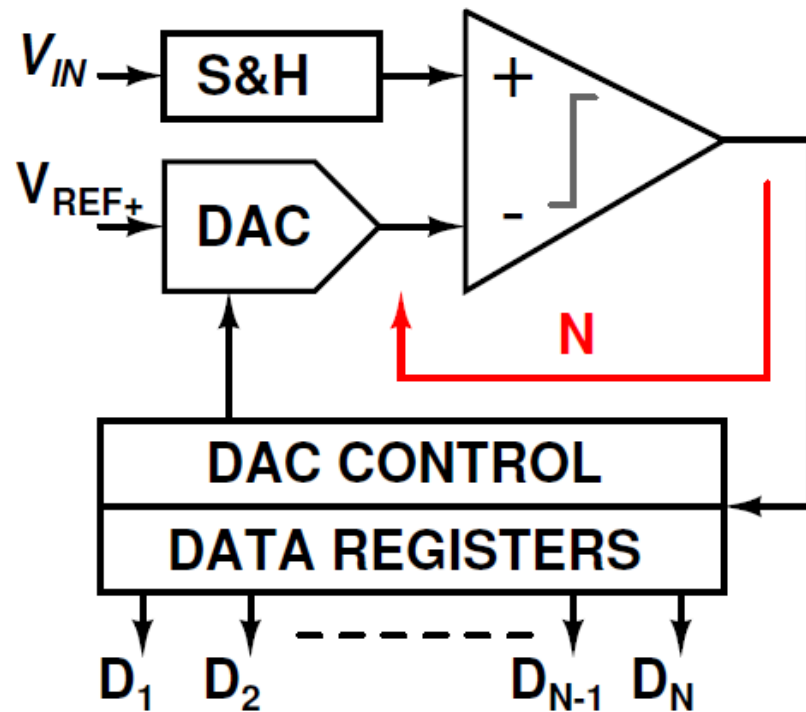


Figure: Block diagram of a successive approximation register ADC 13

- Serial processing ADC
- Lower power consumption for higher resolution
- Medium speed ADC (≤ 100 MHz)
- Conversion cycles = N clock cycles
- Hardware efficient
- Binary search algorithm

Hybrid ADC: Flash and SAR

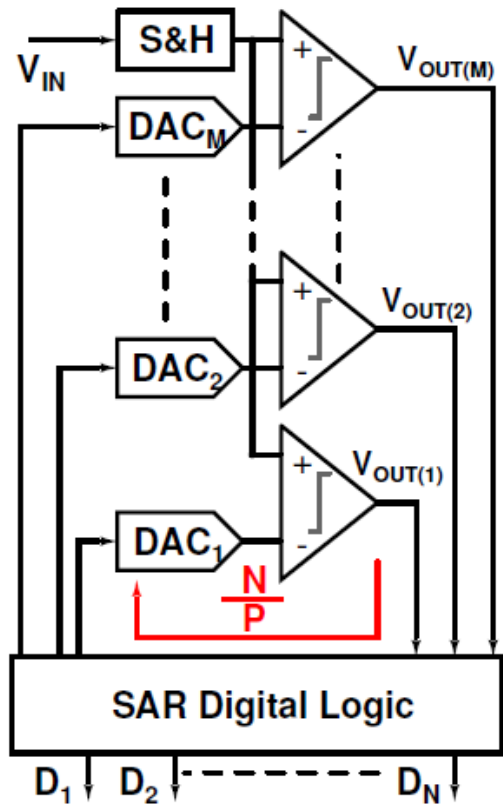


Figure: Block diagram of a hybrid flash-SAR ADC 14

- Binary search algorithm with parallel conversion of partial bits.
- Each cycle produces P bits.
- The search space is divided into $M+1$ ($2^P = M+1$).
- Conversion cycles = $\frac{N}{P}$ clock cycles.
- $2^P - 1$ comparators and DACs.
- Bits per cycle is a trade-off between area and speed.

¹⁴ Seyed Alireza Zahrai and M. Onabajo, "A low-power hybrid ADC architecture for high-speed medium-resolution applications," 2015 IEEE 58th International Midwest Symposium on Circuits and Systems, Aug. 2015, pp. 1-4.

Hybrid Architecture ¹⁵

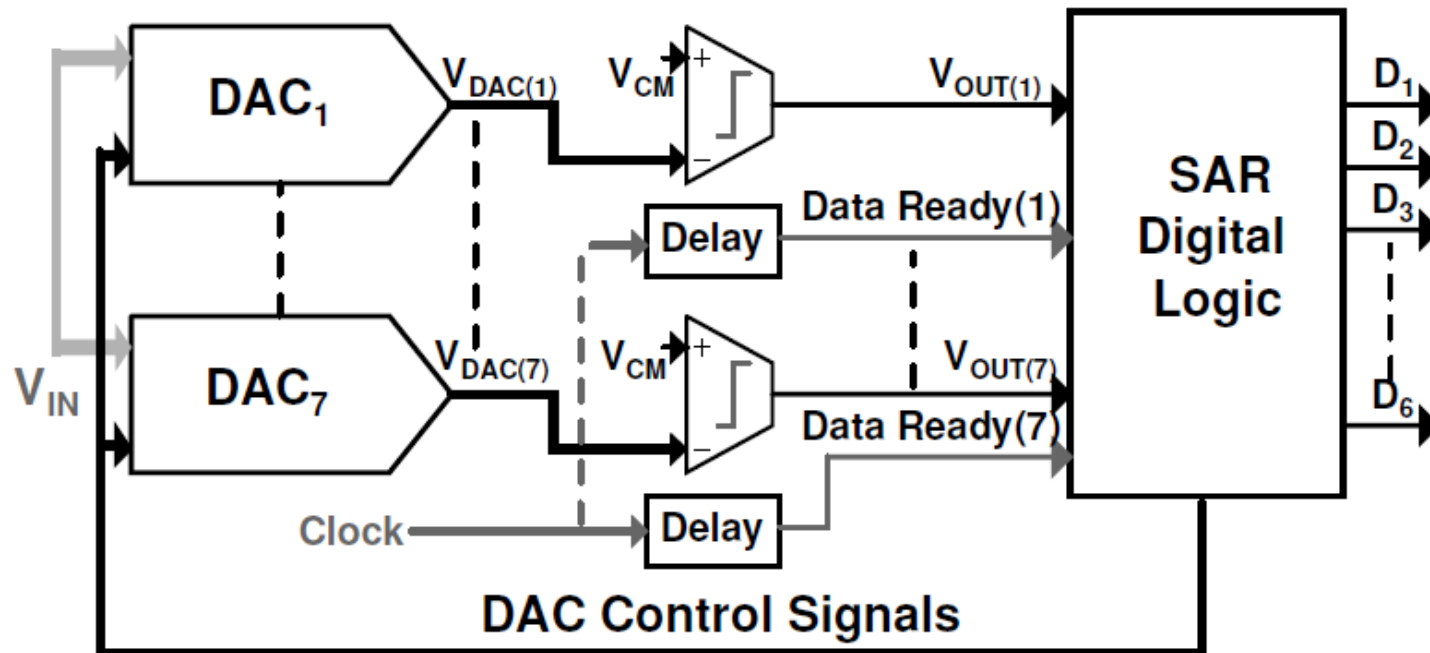


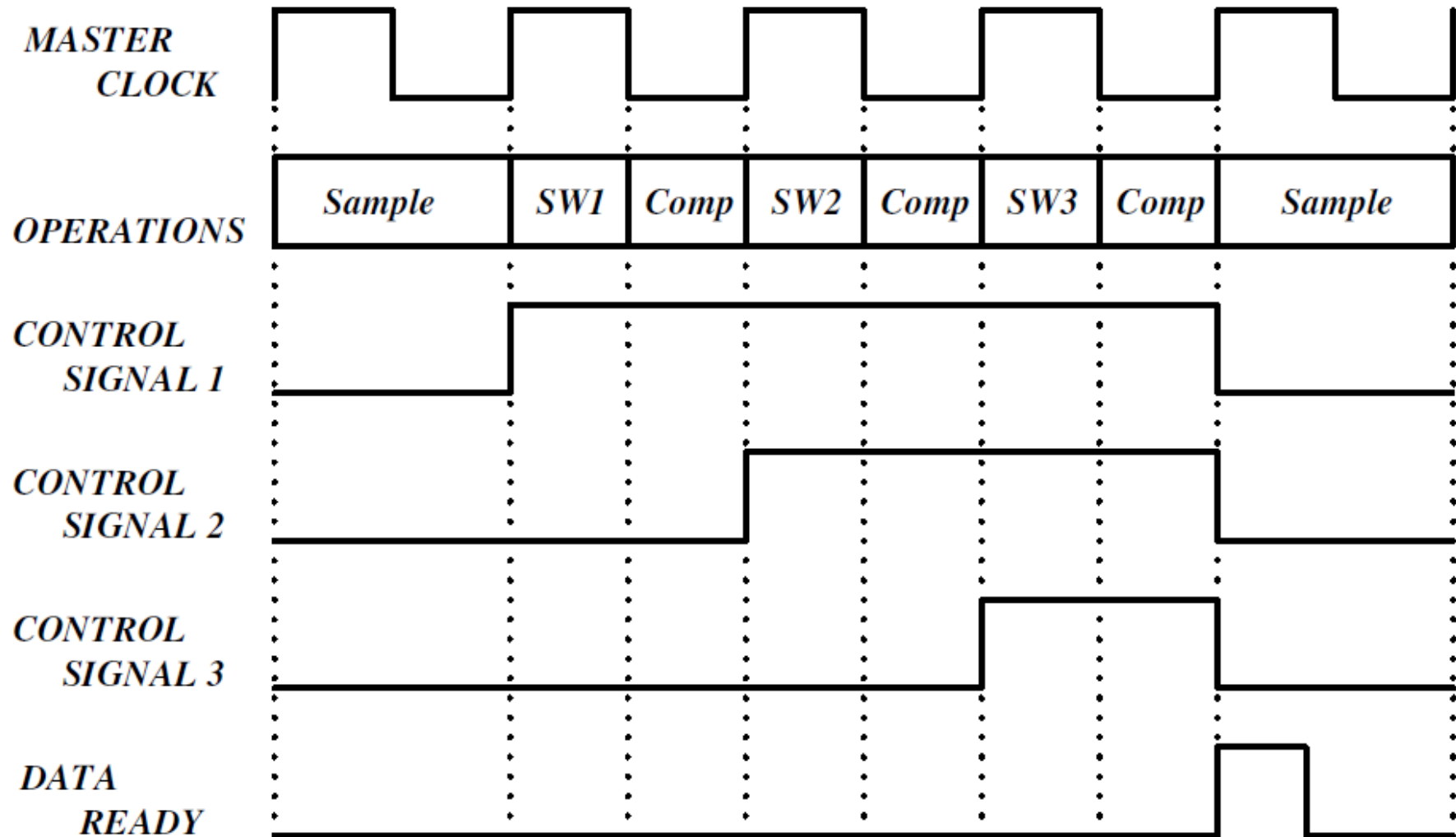
Figure: The block-diagram of a 3-bit per stage, 6-bit flash-SAR ADC.

¹⁵ Dinesh Kumar B. et. al, "Design of Hybrid Flash-SAR ADC using an Inverter based Comparator in 28 nm CMOS", in Elsevier Microelectronics Journal, Volume 95, Jan. 2020, 104666, ISSN 0026-2692.

Salient Features

- A serial SAR ADC combined with a parallel flash ADC.
 - The flash ADC achieves faster operation.
 - The SAR ADC achieves efficient energy conversion.
 - DACs and comparators forms the flash architecture.
 - SAR digital logic forms the SAR loop.
 - Conversion cycle is reduced by $(N/m) + 1$.
 - A 2-bit/cycle architecture is adopted.
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Timing Diagram



SW: Switching operation

Comp: Comparison

Design Specifications

Table: Specifications of the hybrid flash-SAR ADC

Power Supply	0.9 V
Technology Node	28 nm CMOS
Architecture	Hybrid
Speed	1 GS/s
Algorithm	3 bit/cycle
Resolution	6 bits
Power	2.33 mW
FOM ¹¹	47.7 fJ/conv

$$^{11}\$FOM = \frac{\text{Power}}{2^{\text{ENOB}} \times F_c},$$

Specifications

- Comparator
 - Bandwidth = 4 GHz,
 - Resolution = 14 mV,
 - Decision time = 94 ps.
 - Digital logic
 - Clock Control,
 - DAC Control,
 - Thermometric to binary encoder,
 - Memory unit.
 - Segmented split capacitor DAC
 - Resolution = 14 mV,
 - Speed = 4 GHz,
 - Unit capacitance = 8 fF,
 - Settling time = 20 ps.
-
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Inverter based Comparator

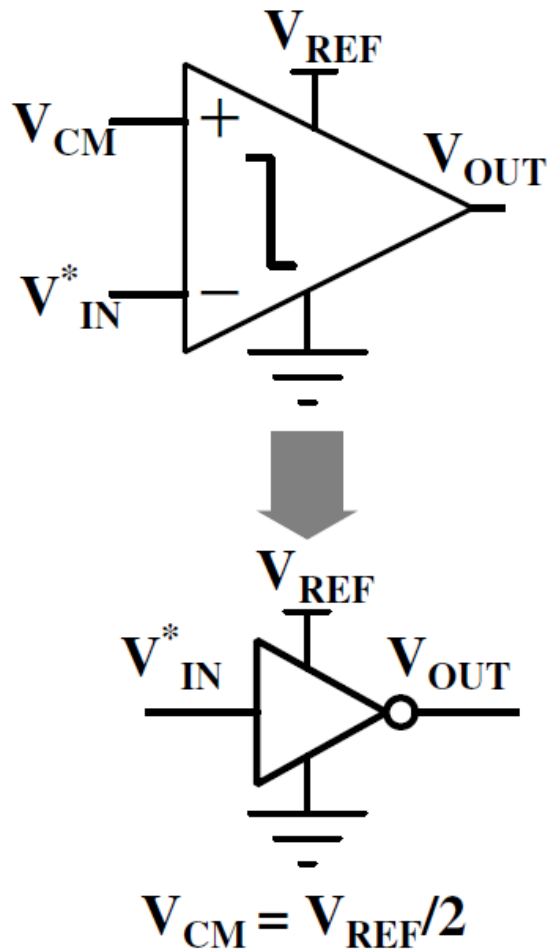


Figure: Idea of inverter based comparator.

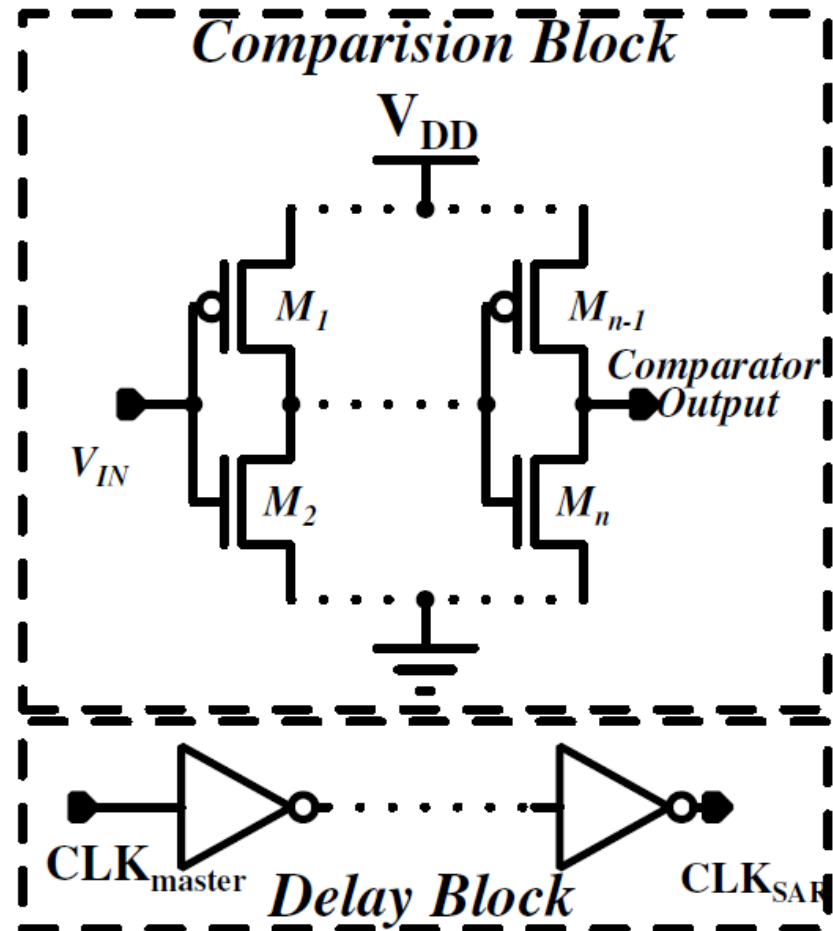


Figure: The schematic of inverter based comparator.

Common Mode Feedback (CMFB)

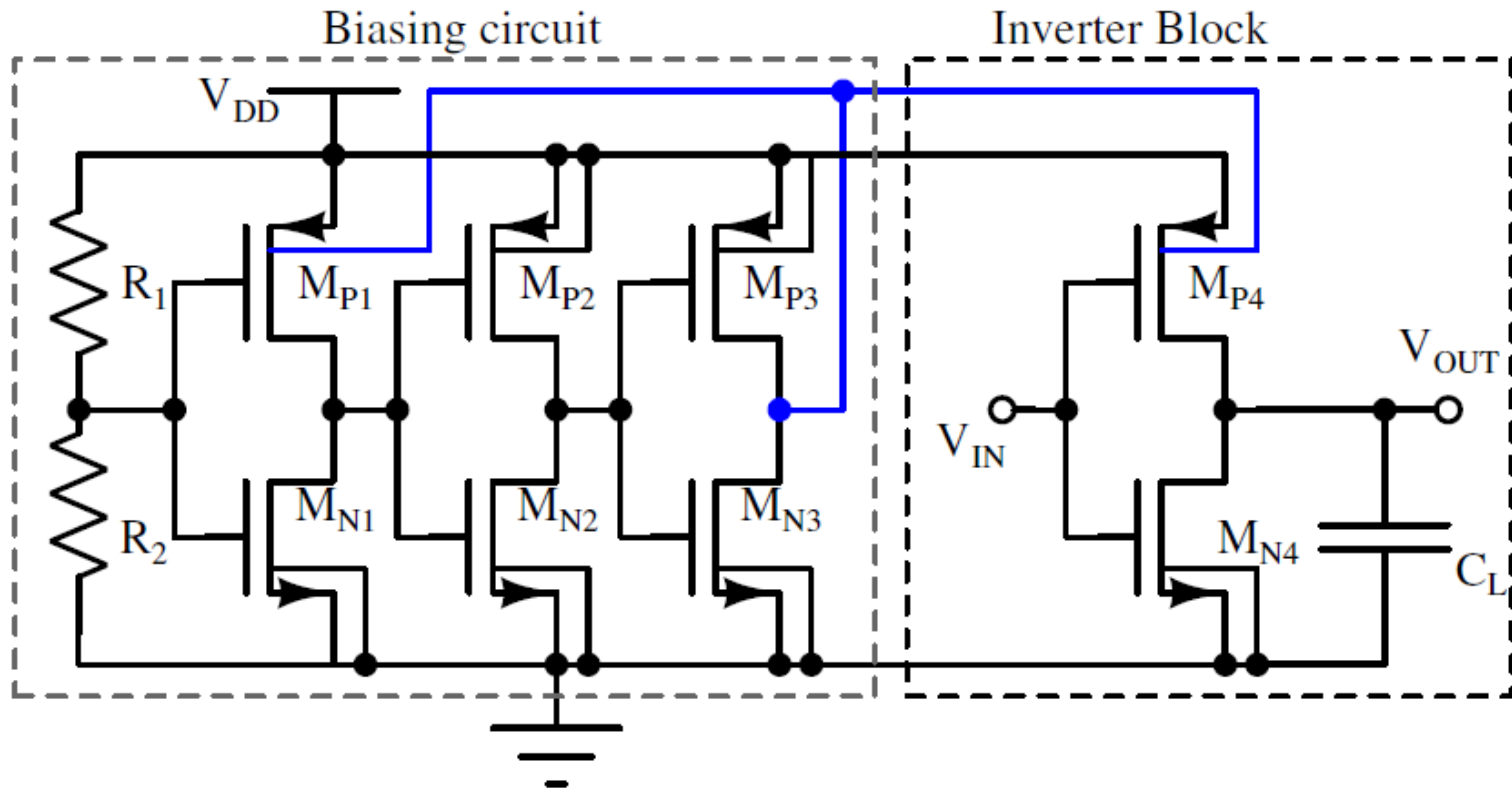


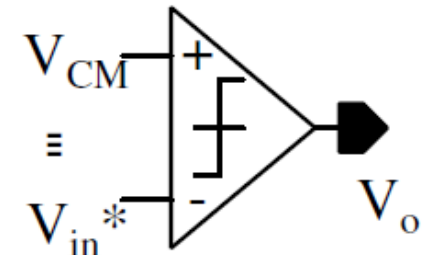
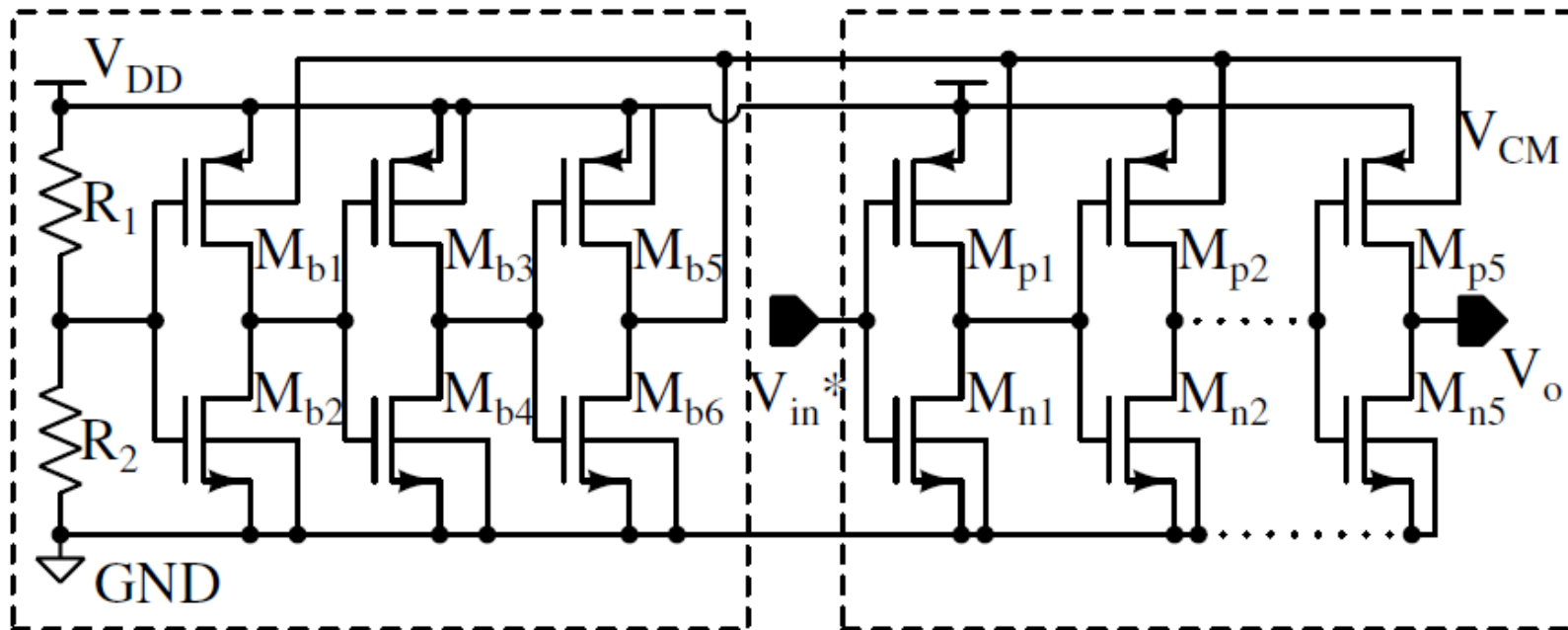
Figure: VCM compensated single stage inverter based comparator ¹⁶.

¹⁶ H. Shrimali and S. Chatterjee, "11 GHz UGBW Op-amp with feed-forward compensation technique", in IEEE ISCAS, May 2011

Proposed Inverter based Comparator

CMFB

Inverter based comparator



V_{in}^* : Sampled input

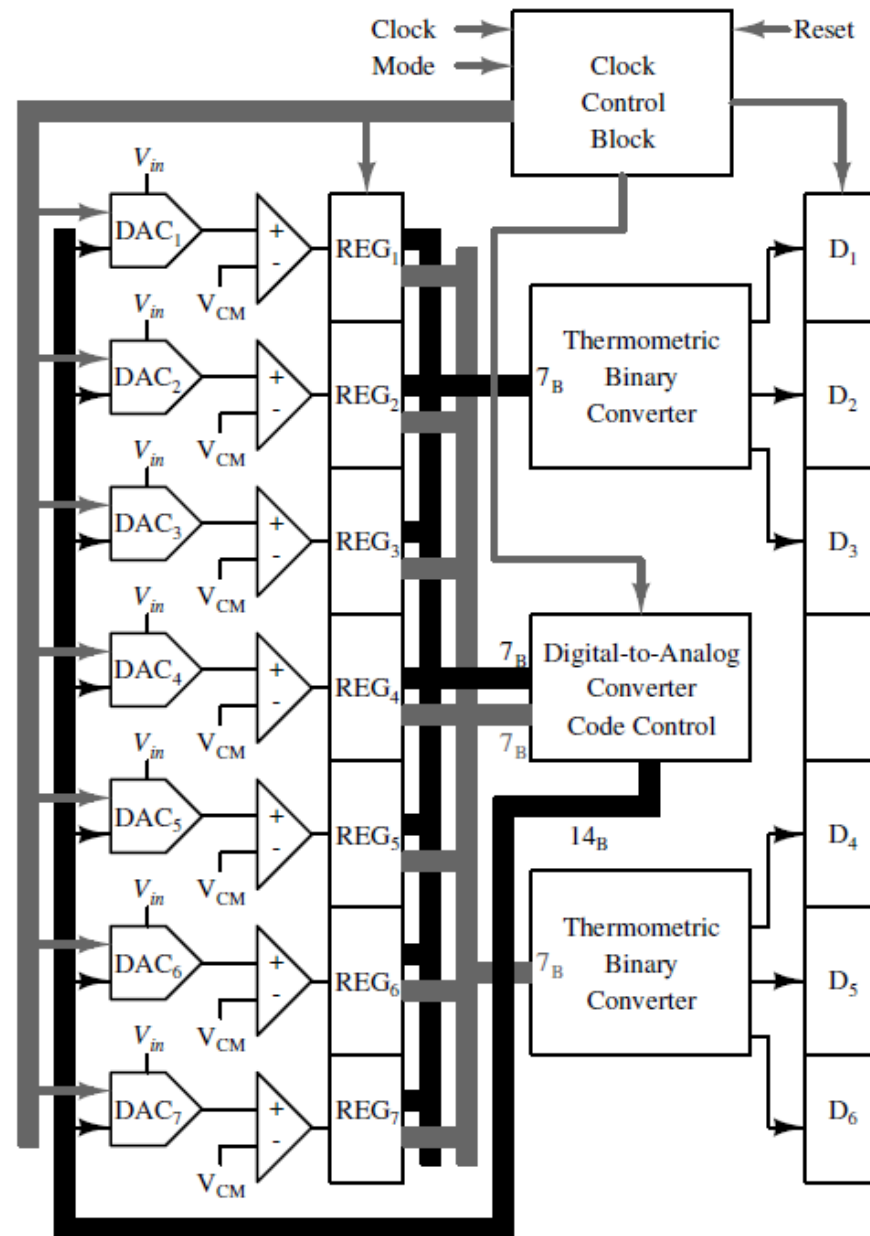
Inverter based Comparator

- An inverter can be used as a comparator, when
 - Switching Threshold = V_{CM} .
- Common-mode-feedback (CMFB) circuitry for fixing the V_{CM} ¹⁶ across PVT variations.
- Input offset voltage requirements can be achieved with a chain of inverters in cascade¹⁷
- The δ delay for data ready is created using chain of inverters.

¹⁶ H. Shrimali and S. Chatterjee, "11 GHz UGBW Op-amp with feedforward compensation technique," in IEEE ISCAS, May 2011, pp. 17– 20.

¹⁷ I. Sutherland, et.al, Logical Effort: Designing Fast CMOS Circuits. San Francisco, CA, USA: Morgan Kaufmann Publishers Inc., 1999.

Power Aware 3bit/cycle ADC



Charge Scaled DAC (CDAC)

- The CDAC converts the digital input to an analog voltage.
 - The CDAC decides the
 - Integral Non Linearity (INL)
 - Differential Non Linearity (DNL)
 - Signal to Noise Ratio (SNR)
 - Inherent sample and hold circuit
 - No static power consumption
 - Bottom plate sampling to avoid parasitic effects
 - Capacitance spread of DAC increases with number of bits
 - Lower switch resistance
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CDAC Architectures

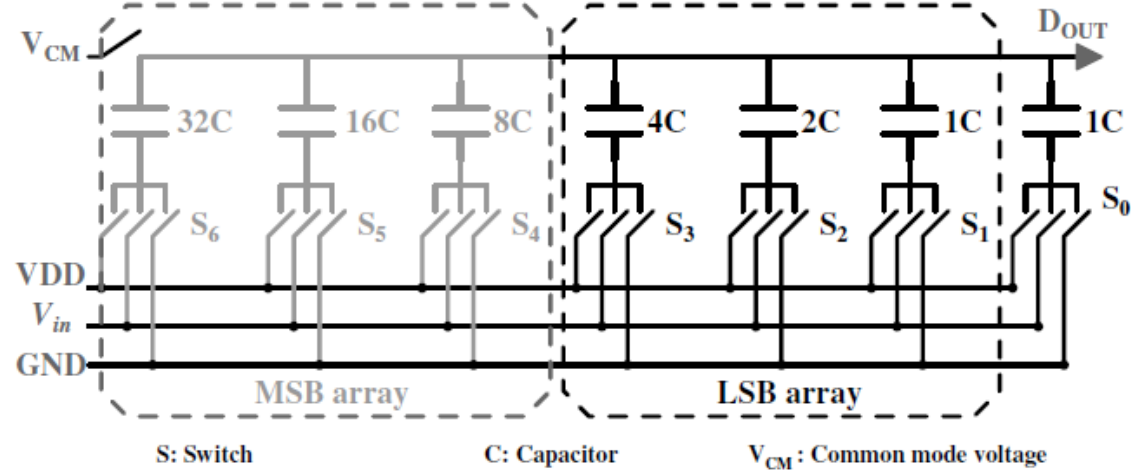


Figure: Conventional CDAC architecture.

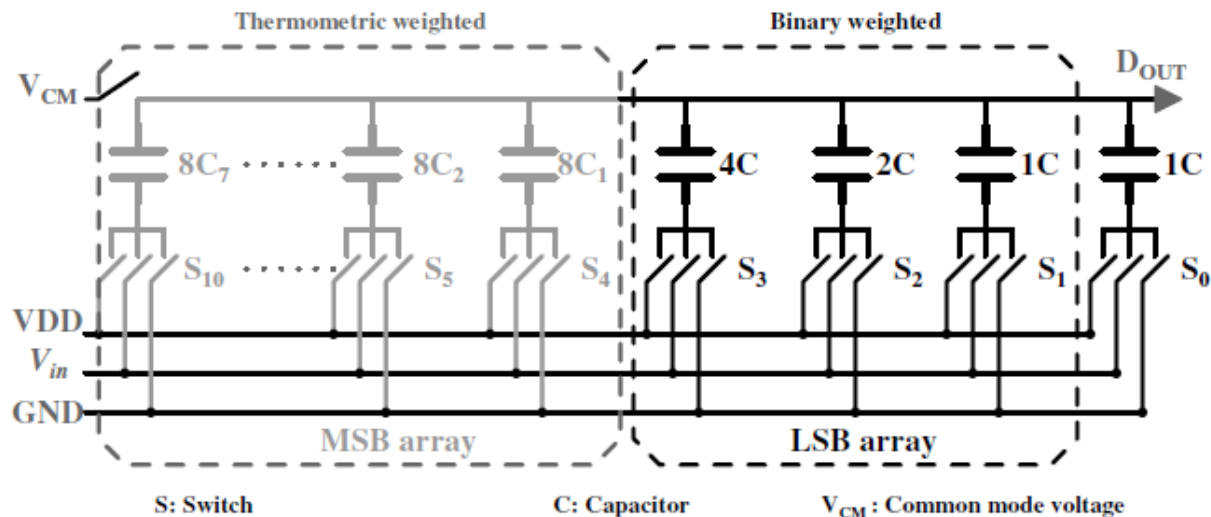


Figure: Segmented CDAC.

Proposed CDAC

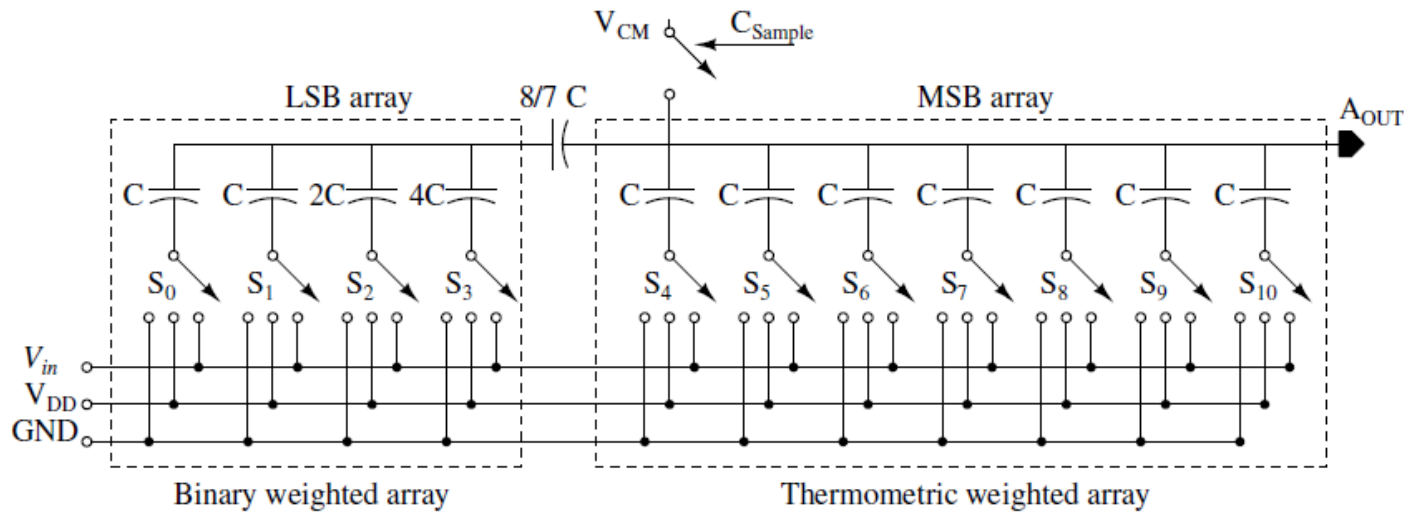
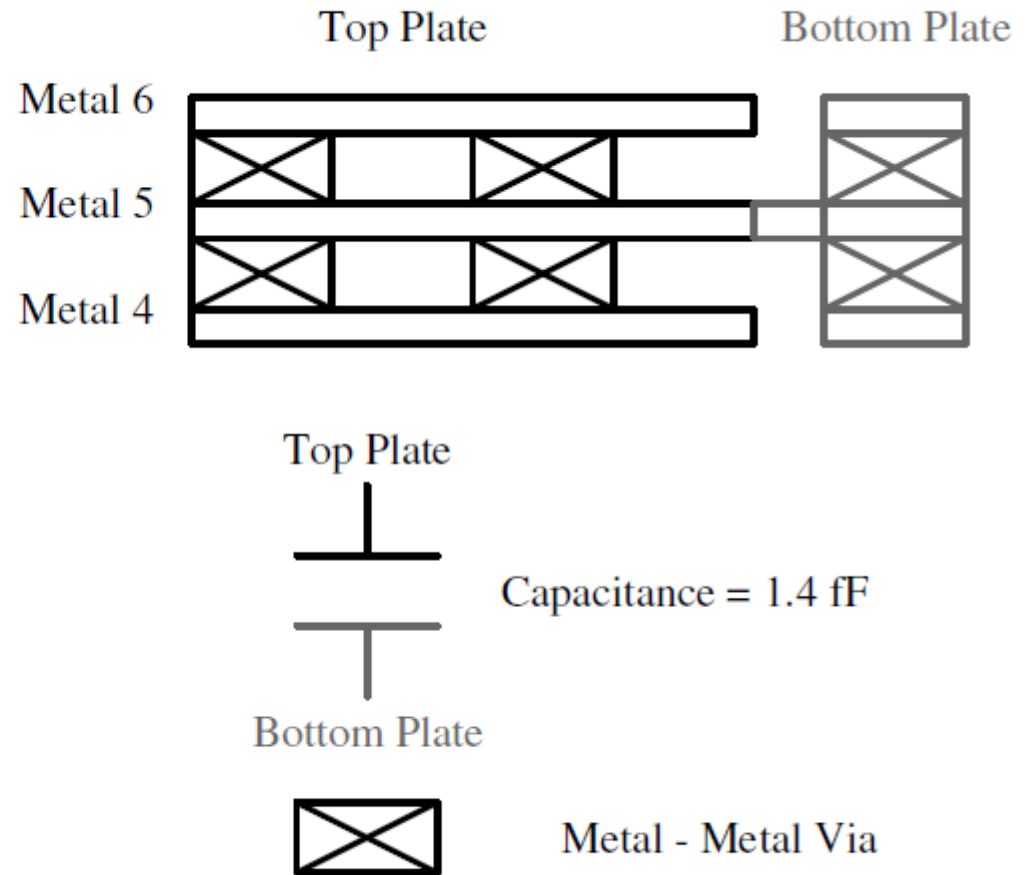
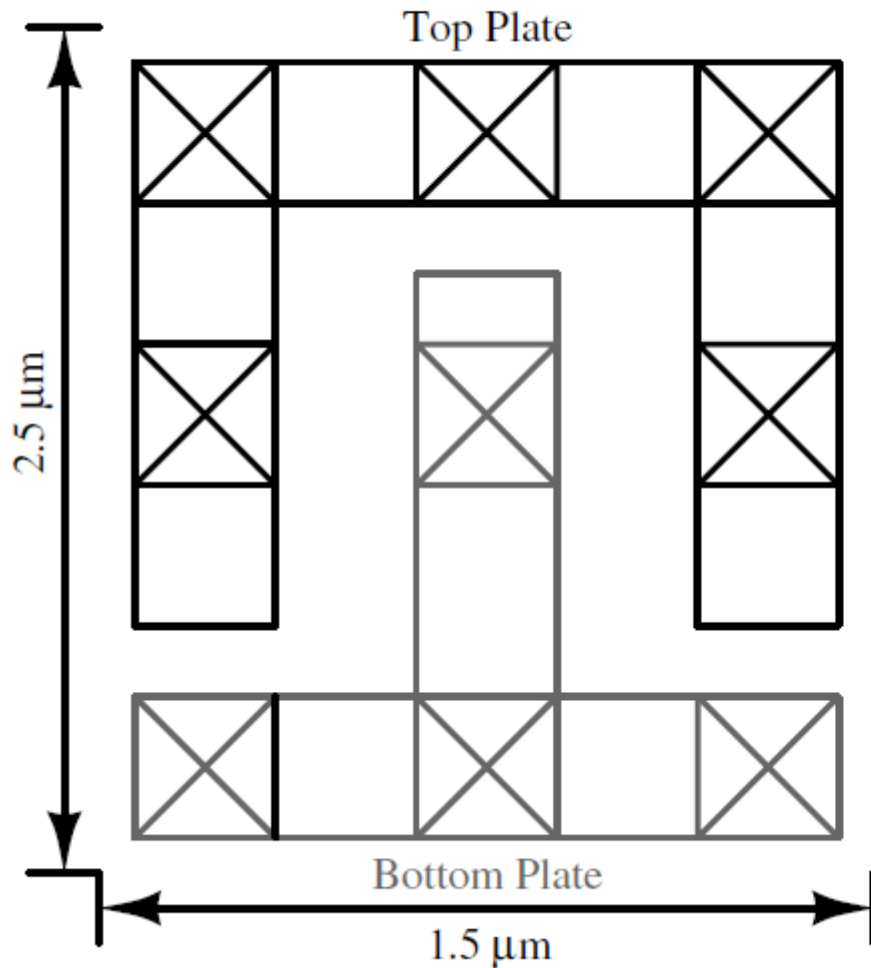


Figure: Implemented segmented split-capacitor array CDAC.

- 87% reduction in area
- Reduced capacitance spread
- Increased speed
- Requires only simple switch circuit.

Custom Capacitance: UMC130



Results (28nm CMOS)

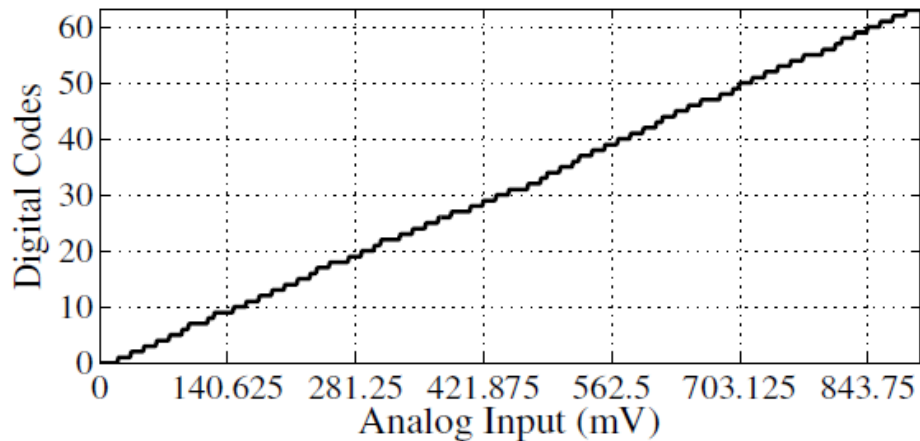


Figure: I/O characteristics for ADC.

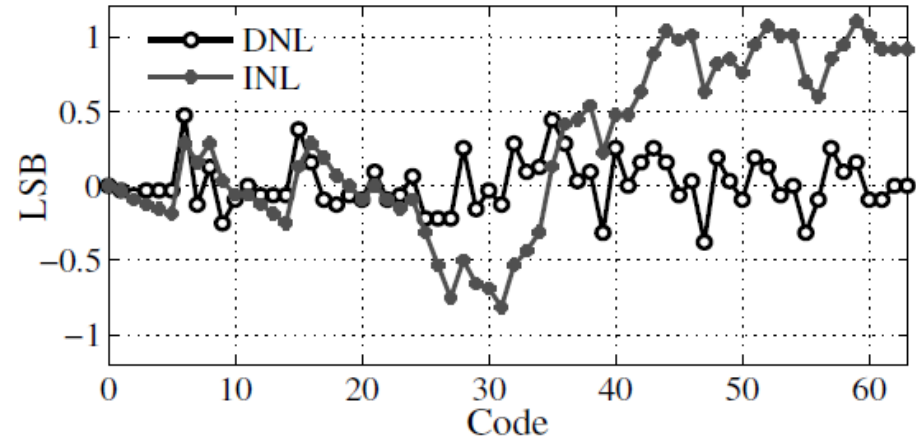


Figure: INL/DNL plots for the ADC.

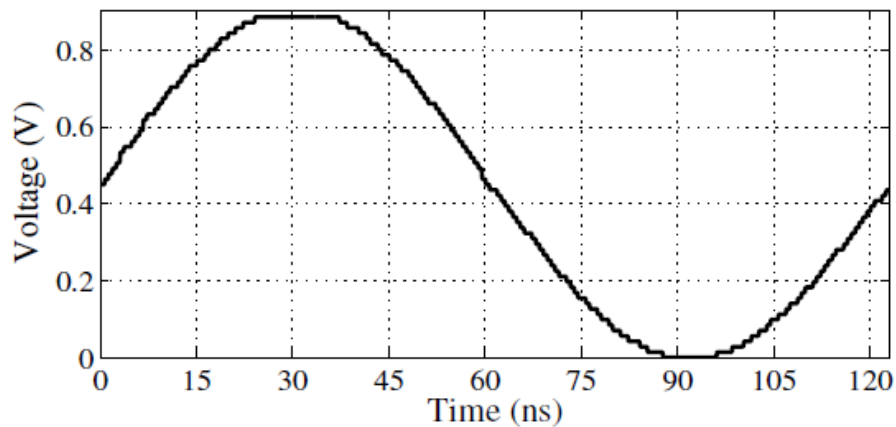


Figure: Transient response of the ADC.

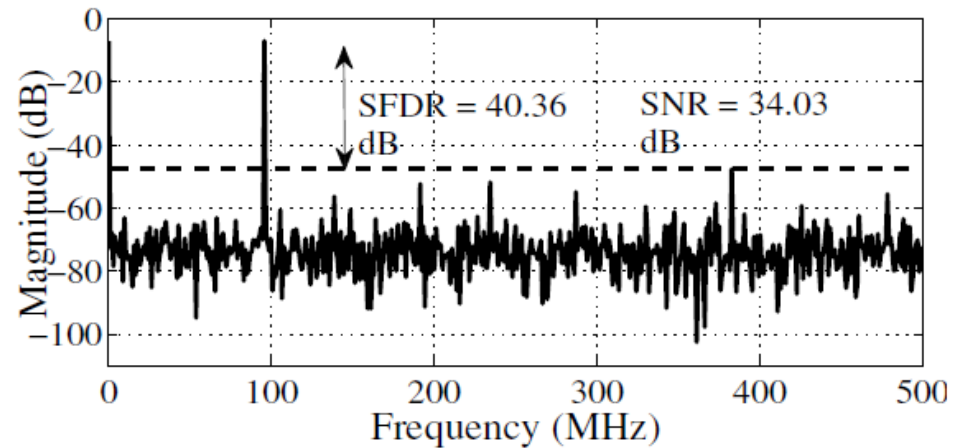


Figure: 1024-point FFT

Results (28nm CMOS)

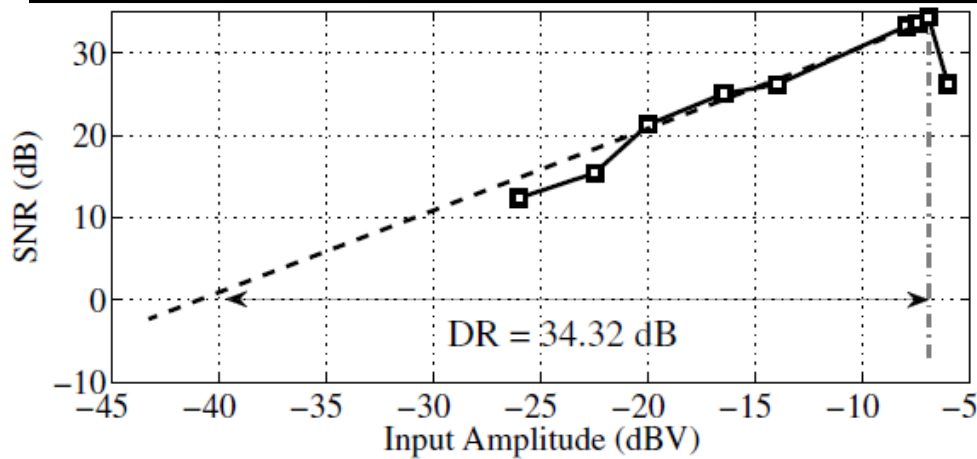


Figure: Variation of the SNR with input signal amplitude for a 1 MHz sinusoid.

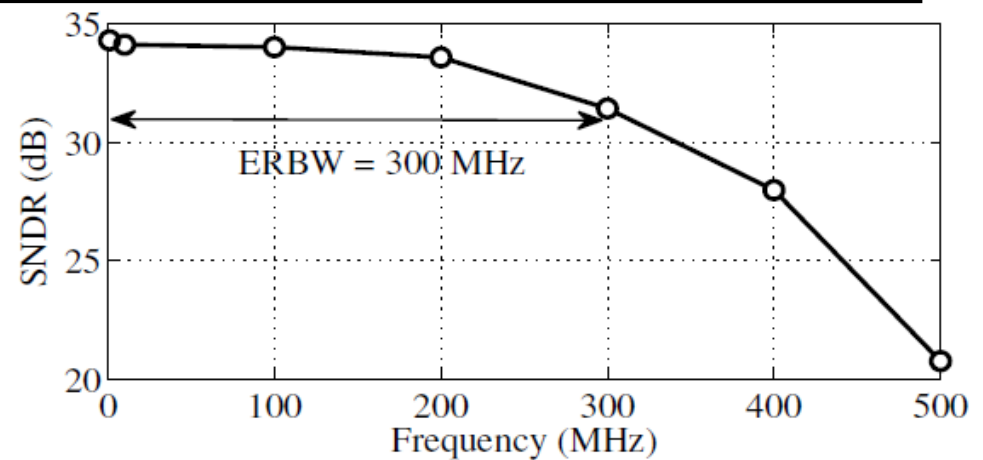


Figure: Variation of SNDR with input signal frequency.

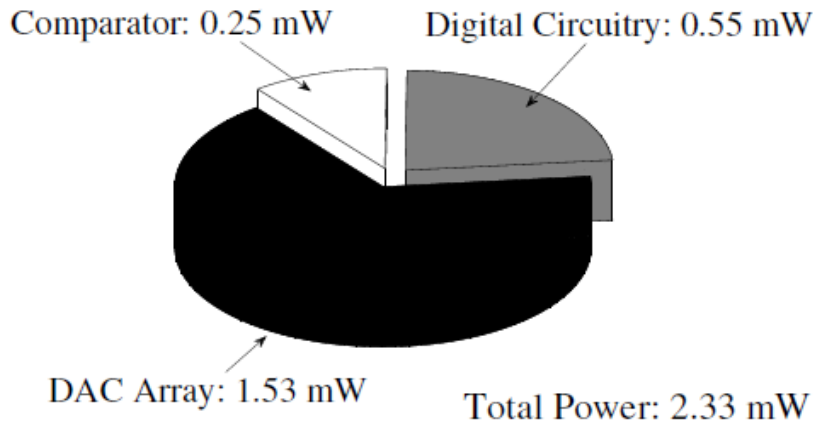


Figure: Power consumption of various sub-blocks of the ADC.

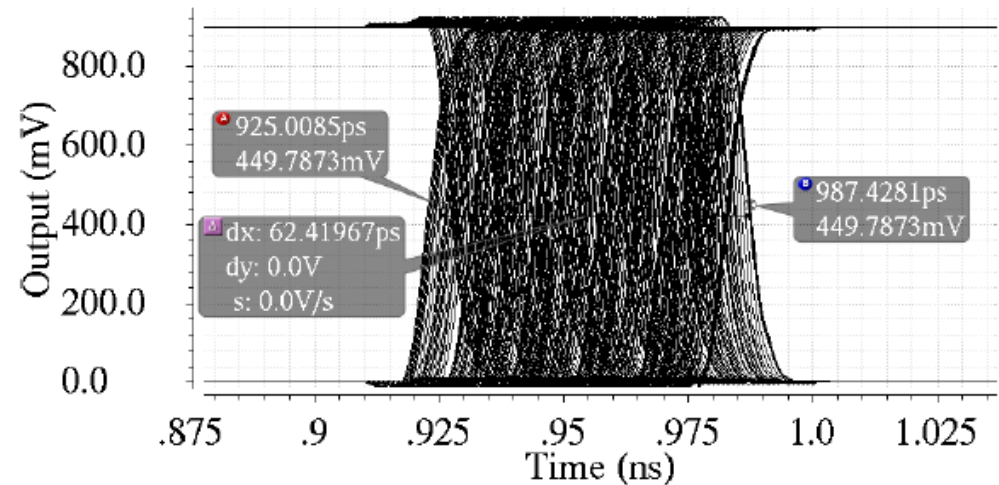


Figure: Eye diagram of the MSB with PRBS of 10 ns bit period.

Results (28nm CMOS)

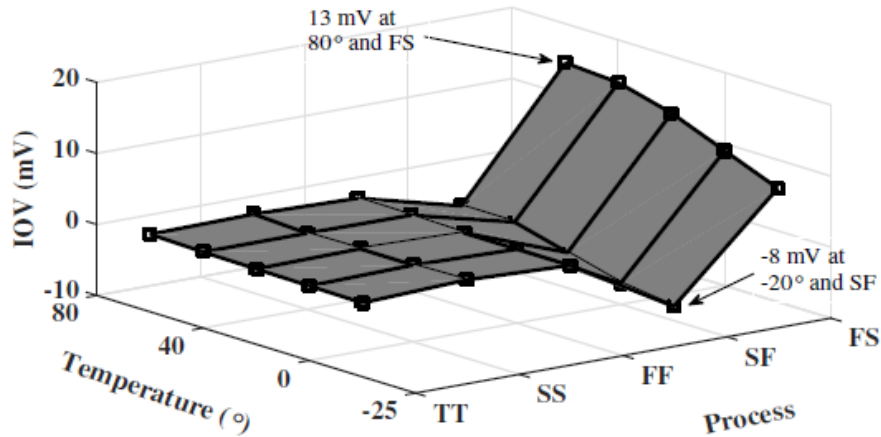


Figure: Variation of input offset voltage (IOV) with process and temperature corners.

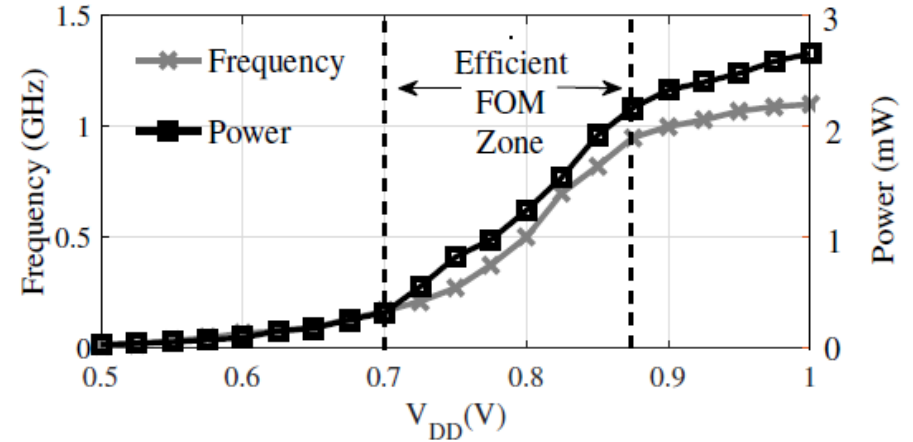


Figure: The speed and power behavior with respect to varying V_{DD} .

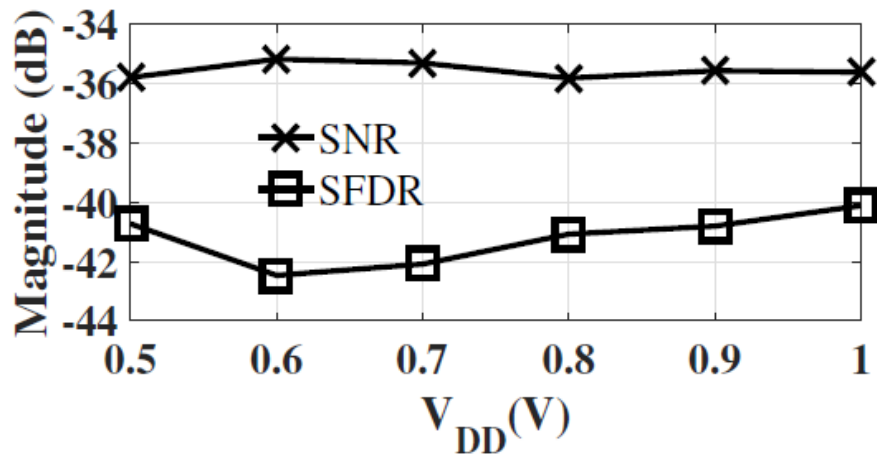


Figure: The SNR and SFDR variations with respect to V_{DD} .

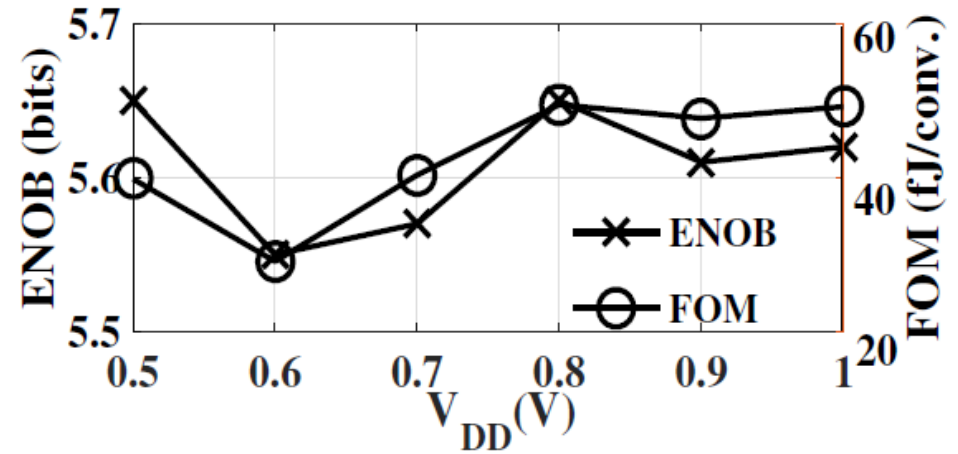


Figure: The ENOB and FOM variations with respect to V_{DD} .

Comparison

Table: Comparison with the state-of-the-art works.

	Technology (nm)	V_{DD} (V)	Architecture	ENOB (Bits)	F_s (GHz)	SNDR (dB)	Power (mW)	Conversion cycles	FOM (fJ/conv) ^a
18 *	55	1.2	SAR	5.6	1.6	35.4	5	7	64
19 *	65	–	2b/cy SAR	5.9	0.32	37.20	9.81	4	479
20 *	180	1.8	SAR	5.87	0.30	36.02	0.64	7	36.47
21)*	180	1.8	FLASH	3.6	0.40	23	0.95	1	190
This work	28	0.9	3b/cy SAR	5.61	1	35.56	2.33	3	47.7
This work	28	0.6	3b/cy SAR	5.55	0.06	35.18	0.01	3	29.56

^aFOM = $\frac{\text{Power}}{2^{\text{ENOB}} \times F_s}$, * Simulation results.

18 Y. H. Chung and W. S. Rih, "A 6-bit 1.6-GS/s domino-SAR ADC in 55nm CMOS," in ISOCC, Nov. 2017, pp. 216–217.

19 W. Xu, Q. Wei, L. Luo, and H. Yang, "A 6-bit 320-MS/s 2-bit/cycle SAR ADC with tri-level charge redistribution," in IEEE ASID, Sep. 2015, pp.71–75.

20 A. Bekal, et.al, "Sixbit, reusable comparator stage-based asynchronous binary-search SAR ADC using smart switching network," IET Circuits, Devices Systems, vol. 12, no. 1, pp. 124–131, 2018.

21 H. Molaei and K. Hajsadeghi, "A low-power comparator-reduced flash ADC using dynamic comparators," in IEEE ICECS, Dec. 2017, pp. 5–8

Summary: Design

- Supply voltage scalability characteristics.
 - Biasing circuitry for fixing V_{CM} across PVT variations.
 - Optimum unit capacitor selection for segmented split capacitor DAC.
 - Desired sampling rate for efficient FOM.
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Jitter Perspectives

- The demand for low power, high speed and robust circuits is increasing in the current scenario.
- Power consumption and speed specifications are crucial for high speed mixed signal systems ²²
- Maintaining the signal integrity (SI) and power integrity (PI) are the major bottlenecks
- The primary sources of jitter are
 - Power supply noise (PSN),
 - Substrate noise,
 - Process variations,
 - Crosstalk,
 - Electromagnetic interference (EMI), *etc* ²³

²² J. Fang, S. Thirunakkarasu, X. Yu, F. Silva-Rivas, C. Zhang, F. Singor and J. Abraham, A 5 GS/s 10-b 76 mW time-interleaved SAR ADC in 28 nm CMOS, IEEE Transactions on Circuits and Systems I: Regular Papers, vol. 64, no. 7, pp. 16731683, Jul. 2017

²³ K. Oh and X. Yuan, HighSpeed Signaling: Jitter Modeling, Analysis and Budgeting. Prentice Hall, 2011.

VCM compensated Comparator

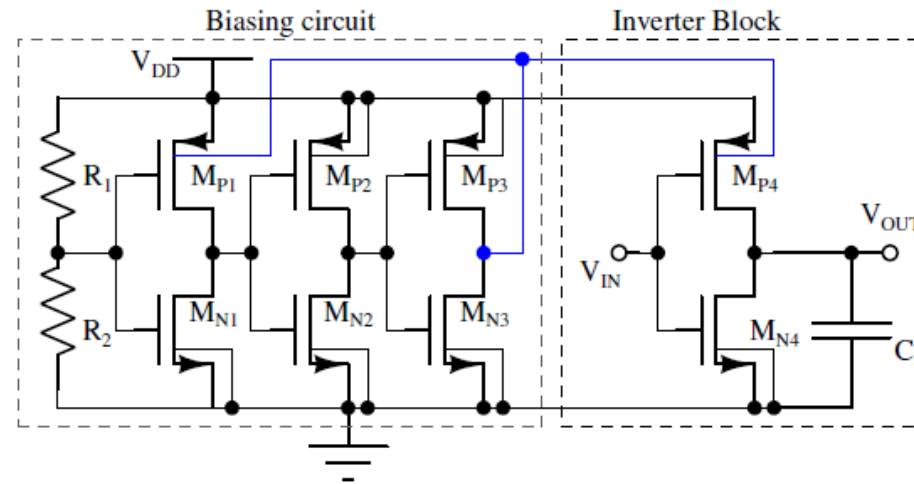


Figure: VCM compensated inverter based comparator with W/L ratios are $M_{N1} = M_{N4} = (0.3\mu m/0.09\mu m)$, $M_{P1} = M_{P4} = (0.51\mu m/0.09\mu m)$, $M_{N2} = M_{N3} = (0.1\mu m/0.03\mu m)$, $M_{P2} = M_{P3} = (0.17\mu m/0.03\mu m)$.

The output of the comparator (V_{OUT}) is decided by the switching threshold voltage V_{sw} and is given as:

$$V_{sw} = V_{DD} \frac{r_{ON_N}}{r_{ON_N} + r_{ON_P}}; \quad (1)$$

Small Signal Model

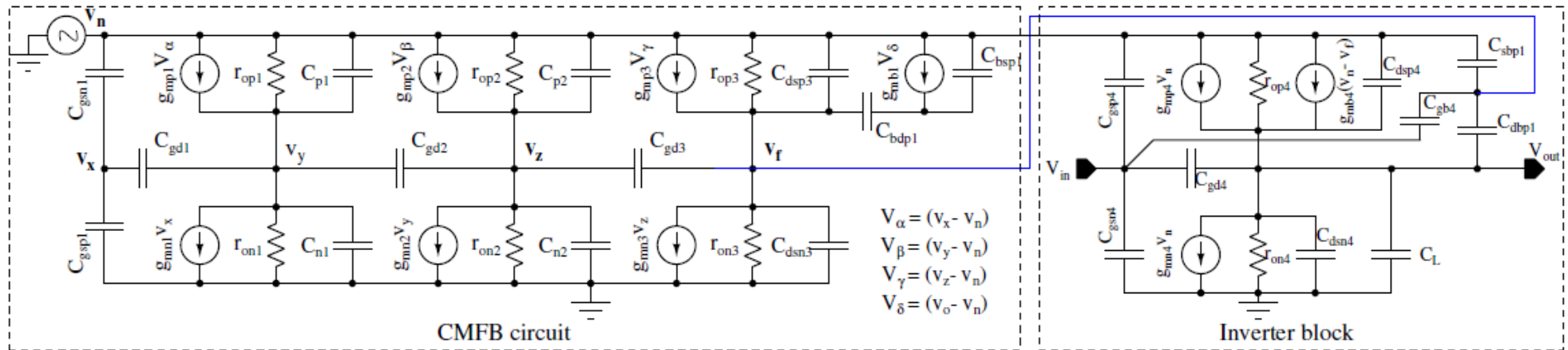


Figure: Small signal model for the VCM compensated inverter based comparator (Fig. 1) in presence of power supply fluctuations.

- The fluctuations in the power supply is transferred to the body of the pMOS transistors and further give rise to PSIJ for the inverter based comparator.
- The admittance matrix method ' ' is one of the useful method to solve circuits with large number of nodes.

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Transfer Function

The transfer function of a system is defined as ²⁵

$$\frac{V_f}{V_n} = [C(sI - A)^{-1}B + D]; \quad (2)$$

where,

- v_f is the power-supply,
- v_n is the substrate bounces,
- A is the transfer matrix,
- B is the input matrix,
- C is the output matrix,
- I is the identical matrix and
- D is the transmission matrix.

²⁵ K. Ogata and Y. Yang, Modern control engineering. Prentice hall India, 2002

Admittance Matrix Method

- Transfer matrix A is written by analysing all the incoming and outgoing currents at each node of CMFB circuit.

$$A = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} & Y_{14} & Y_{15} \\ Y_{21} & Y_{22} & Y_{23} & Y_{24} & Y_{25} \\ Y_{31} & Y_{32} & Y_{33} & Y_{34} & Y_{35} \\ Y_{41} & Y_{42} & Y_{43} & Y_{44} & Y_{45} \\ Y_{51} & Y_{52} & Y_{53} & Y_{54} & Y_{55} \end{bmatrix},$$

- B Matrix is the input current with respect to the output,

$$B = \begin{bmatrix} g_{mp1} \left(\frac{R_2}{R_1 + R_2} - 1 \right) + sC_{gd1} \\ \kappa_2 + g_{mp2} + sC_{gd2} \\ \kappa_3 + g_{mp3} + sC_{gd3} \\ \kappa_4 + g_{mb1} + sC_{db1} \\ -g_{mp1} - g_{mp2} - g_{mp3} - g_{mb1} \\ \kappa_1 - \kappa_2 - \kappa_3 - \kappa_4 \end{bmatrix},$$

- C matrix is due to the current at the output due to input,

$$C = [0 \ 0 \ 0 \ 0 \ 1],$$

D is a null matrix as there is no feed forward element from input to output in CMFB circuit.

EMPSIJ Method

- 1 Transfer function realisation using admittance matrix method

$$\frac{V_f}{V_n} = [C(sI - A)^{-1}B + D]; \quad (3)$$

where A is the transfer matrix, B is the input matrix, C is the output matrix, I is the identical matrix and, D is the transmission matrix

- 2 EMPSIJ²⁶ method for power supply induced jitter estimation

$$J_r = \text{TIE} = \frac{\Delta V_{out}}{\gamma}; \quad (4)$$

where, γ is the slope of rising or falling edge of the comparator output at nominal supply voltage (V_{DD}).

²⁶ J. N. Tripathi, R. Achar, and R. Malik, "Efficient modeling of power supply induced jitter in voltage-mode drivers (EMPSIJ)", IEEE Transactions on Components, Packaging and Manufacturing Technology, Oct 2017.

Power Supply Induced Jitter

The output of the comparator due to noise can be expressed as:

$$\Delta V_{out} = \frac{(g_{mp4} + g_{mb4} + g_{dsp4})v_n + (sC_{dbp4} - g_{mb4})v_f}{g_{dsp4} + g_{dsn4} + s(C_{gd4} + C_{dbp4} + C_{dsn4} + C_L)}; \quad (5)$$

where, $g_{dsp4} = r_{op4}^{-1}$ and $g_{dsn4} = r_{on4}^{-1}$.

The closed-form expression for PSIJ can be formulated using:

$$J_r = \frac{(g_{mp4} + g_{mb4} + g_{dsp4})v_n + (sC_{dbp4} - g_{mb4})v_f}{\gamma(g_{dsp4} + g_{dsn4} + s(C_{gd4} + C_{dbp4} + C_{dsn4} + C_L))}; \quad (6)$$

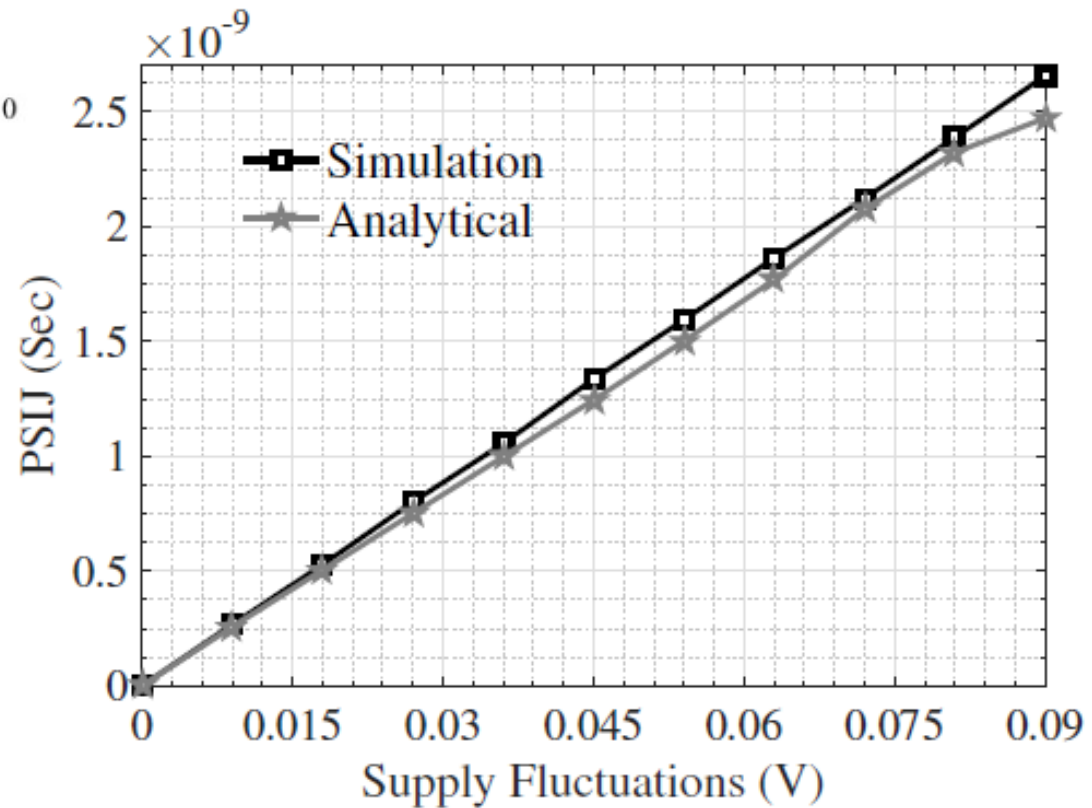
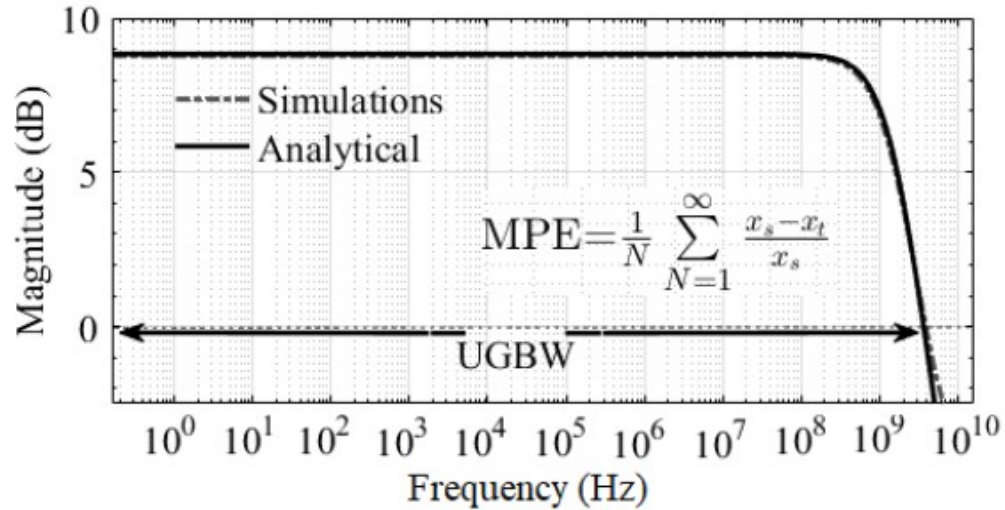
where, $C_{gd4} = C_{gdn4} + C_{gdp4}$.

Next, the peak-to-peak value of PSIJ can be calculated using the following relationship:

$$\text{PSIJ} = \max\{J_r^k\}_{k=1}^n - \min\{J_r^k\}_{k=1}^n, \quad (7)$$

where J_r^k is the TIE at k^{th} rising or falling edge.

Results



Summary: Model

- The proposed model is in agreement with simulation results.
 - Impact of jitter is observed in presence of substrate noise.
 - PSIJ shows linear increment and can affect SNR.
 - Model can be extended for ground noise.
 - Method can be extended for analog and digital circuits.
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Key References

- **Journal**

- ① Dinesh Kumar B, Sumit K. Pandey, Navneet Gupta and Hitesh Shrimali " Design of Hybrid Flash-SAR ADC using an Inverter based Comparator in 28 nm CMOS" , Microelectronics Journal .

- **Conference**

- ① Dinesh Kumar B, Navneet Gupta, Hitesh Shrimali " A 6-bit, 29.56 fJ/conv-step, Voltage Scalable Flash-SAR Hybrid ADC in 28 nm CMOS" , in IEEE ISCAS, May 2019.
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सत्यमेव जयते

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Thank you!
